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# A Study of a Steel Right Circular Cylinder (RCC) Striking 23 Plies of KM2 Fabric Using the LS-DYNA Lagrangian Hydrocode

by Dennis S. Pritchard

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# **Army Research Laboratory**

Aberdeen Proving Ground, MD 21005-5066

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## **A Study of a Steel Right Circular Cylinder (RCC) Striking 23 Plies of KM2 Fabric Using the LS-DYNA Lagrangian Hydrocode**

Dennis S. Pritchard

Weapons and Materials Research Directorate, ARL

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## **Abstract**

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A study was conducted to examine the terminal effects of a 1.0-g steel RCC impacting 23 plies of KM2 fabric using the LS-DYNA Lagrangian hydrocode. The simulated impact velocities were 200, 400, 600, 800, 1000, 1200, and 1400 m/s. The fabric was a plain weave of 850 denier yarn. The LS-DYNA-simulated  $V_s$  versus  $V_t$  data points generated at the U.S. Army Research Laboratory (ARL) were compared to both experimental data and EPIC-generated data. Also, the LS-POST software package was used to view the simulated physical descriptions of the penetrator and target at various stages of the penetration process.

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## Acknowledgments

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This work was supported in part by a grant of computer time from the DOD High Performance Computing Modernization Program at Aberdeen Proving Ground, MD. Mr. D. Grove is gratefully acknowledged for his efforts in support of the work reported here.

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## 1. Introduction

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A study was conducted to examine the terminal effects of a 1.0-g steel right circular cylinder (RCC) impacting 23 plies of KM2 fabric. Simulations and analyses were conducted using the LS-DYNA Lagrangian hydrocode\* in support of the Science and Technical Objective (STO) titled "Ballistic Protection for Improved Individual Survivability." This joint STO between the U.S. Army Research Laboratory (ARL) and the Natick Soldier Center is advancing materials technology to improve the protection of personnel armor systems against current and emerging fragment and bullet threats. The STO is also providing tools to benefit the development, design, and acquisition of personnel armor.

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## 2. Review and Analysis

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Experimental  $V_s$  (striking velocity) versus  $V_r$  (residual velocity) data and hydrocode simulations using LS-DYNA and EPIC are discussed in the following sections.

### 2.1 Experimental Data

Experimental data forms the baseline for comparison to the computed results. The experimental data from Johnson et al. (1999) are shown in Figure 1 and Table 1. The RCC, having a length-to-diameter ratio of one, struck the targeted fabric layup at 0° obliquity. It is seen that a  $V_{50}$  of approximately 600 m/s can be assigned to the experimental data. The  $V_{50}$  is defined within a narrow  $V_s$  range as the  $V_s$  that is bracketed by half of the projectiles in a test sampling in that narrow range not making it through the target layup ( $V_r = 0$ ), balanced by a corresponding half number of projectiles barely penetrating the target layup ( $V_r > 0$ ) in the same range. Once the exact "over" and "under" data points are determined, the  $V_{50}$  equals the average of the  $V_s$  values for these points. From an experimental standpoint of obtaining  $V_{50}$  for a particular penetrator and target configuration, this data set is exemplary, as the cost of determining the  $V_{50}$  is roughly proportional to the number of shots fired; the fewer the shots, the lower the cost. The  $V_{50}$  number often forms the decision point describing the acceptability of an armor configuration on a pass/fail basis when attacked by a particular penetrator. For a more rigorous explanation of how to experimentally find a  $V_{50}$ , the military standard MIL-STD-662E (Department of the Army 1992) should be studied. As the  $V_s$  increased, the fabric layup became less effective in stopping the RCC as a function of the fabric's decreasing ability to withstand dynamic loading.

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\* LS-DYNA Version 950d, Livermore, CA: Livermore Software Technology Corporation.

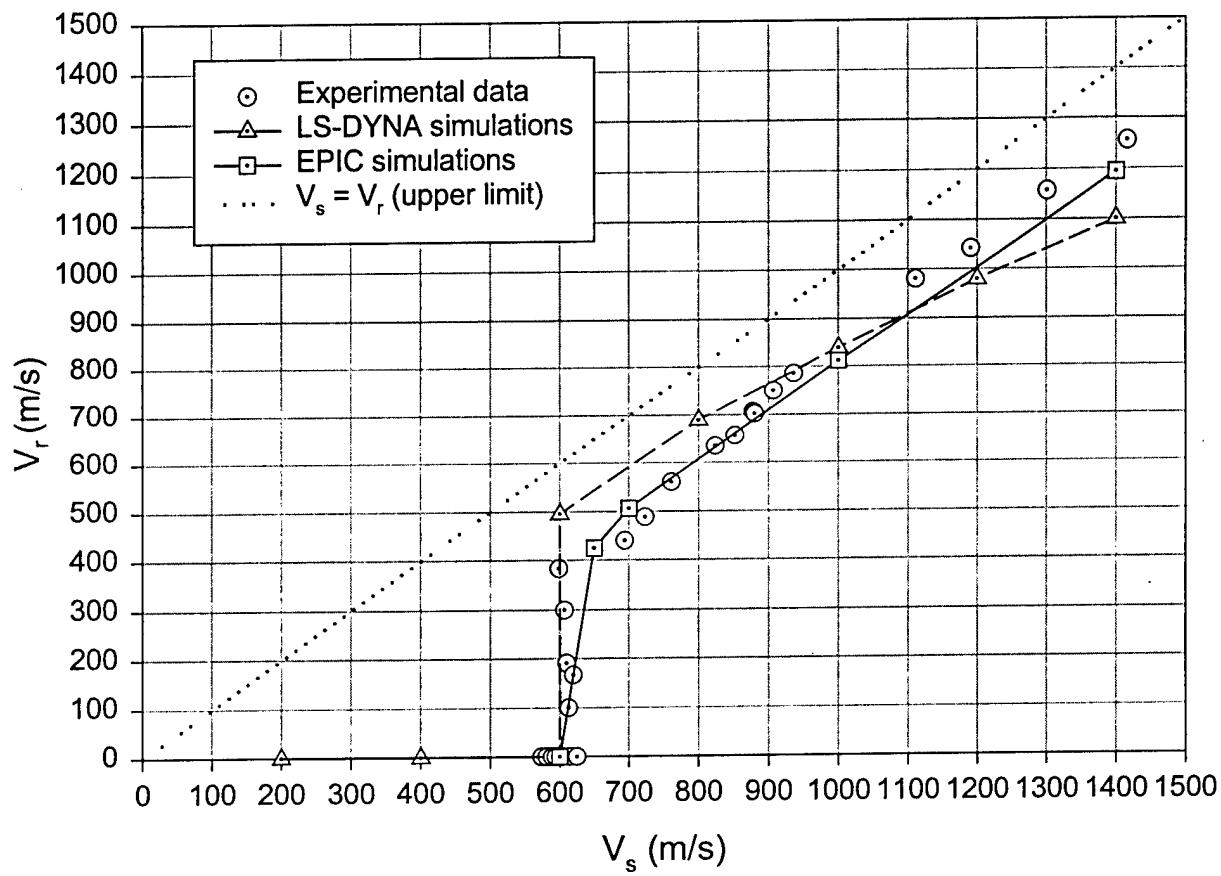


Figure 1. Comparison of simulation results with experimental  $V_s$  versus  $V_r$  data.

Table 1.  $V_s$  versus  $V_r$  values.

Experimental $V_s$ (m/s)	Experimental $V_r$ (m/s)	LS-DYNA $V_s$ (m/s)	LS-DYNA $V_r$ (m/s)	EPIC $V_s$ (m/s)	EPIC $V_r$ (m/s)
574	0	200	0	600	0
581	0	400	0	650	425
589	0	600	495	700	506
594	0	800	689	1000	812
599	383	1000	839	1400	1194
604	0	1200	980		
607	299	1400	1100		
610	191				
615	0				
613	100				
620	167				
625	0				
694	440				
723	488				
761	560				
824	635				
852	656				
878	706				
880	702				
907	750				
936	786				
1111	981				
1191	1042				
1301	1157				
1416	1255				

This statement is evidenced by the increase in  $V_r$  as  $V_s$  increased after the  $V_s$  value of 600 m/s had been significantly surpassed. The  $V_s$  versus  $V_r$  values starting at and including the point with the 599 m/s  $V_s$  value could reasonably be fit with a straight line that roughly parallels the  $V_s = V_r$  line.

## 2.2 LS-DYNA Simulations

The ARL-simulated  $V_s$  versus  $V_r$  data were obtained by using LS-DYNA Version 950d and are shown in Figure 1 and Table 1. The RCC and fabric target grid generation was accomplished by running the LS-INGRID computer software package\* with the ARL-designed input deck presented in Appendix A. This run gave the properly formatted (Fortran 77) node and element data that was stripped from the LS-INGRID output deck called *ingrido*. This stripped deck was inserted into the LS-DYNA keyword formatted deck for each LS-DYNA run, with the material property cards, among others, preformatted. A resultant typical LS-DYNA input deck used in this report, with only the extensive node and element (8-node brick) data abbreviated, is shown in Appendix B. The projectile had a total of 1331 nodes and 1000 solid elements. Each ply had 3362 nodes and 1600 solid elements, with individual element dimensions of  $0.1578 \times 0.5000 \times 0.5000$  mm. The projectile and target element sizing were comparable. Each ply was one element thick, with the ply dimensions equal to  $0.1578 \times 20 \times 20$  mm. Changes were made to the LS-DYNA input deck for each initial impact velocity, where at least each different impact velocity had to be specified, and some changes were required for the other material properties as shown in Table 2.

Table 2. Selected material properties used in LS-DYNA input deck.

Property	KM2 Ply ( $V_s = 200$ and $400$ m/s)	KM2 Ply ( $V_s = 600$ m/s and up)	Steel
Density (g/cm <sup>3</sup> )	1.438 <sup>a</sup>	1.438 <sup>a</sup>	7.87 <sup>b</sup>
Young's Modulus (Mbar)	0.08325	0.74	2.068395 <sup>c</sup>
Poisson's Ratio	0.2 <sup>a</sup>	0.2 <sup>a</sup>	0.29 <sup>d</sup>
Yield Stress (Mbar)	—	—	0.010342 <sup>c</sup>
Failure Strain	0.2	0.025	—

<sup>a</sup> Johnson et al. (1999).

<sup>b</sup> Lyman (1961).

<sup>c</sup> Flinn and Trojan (1975).

<sup>d</sup> Kolsky (1963).

The steel was modeled as an elastic-perfectly plastic material. Although many of the material properties in Table 2 were directly obtained from the listed references, explanations for the choice of others are required as follows.

The KM2 volumetric density in Table 2 was derived from constants found in the Johnson et al. (1999) paper and is close to the commonly quoted value of  $1.44$  g/cm<sup>3</sup>, but is not that exact value. The fabric description was modified from

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\* LS-INGRID Version 3.5, Livermore, CA: Livermore Software Technology Corporation.

the actual weave pattern for each ply into a plate of solid elements with nominally the same material properties as the actual ply. The volumetric density for a simulated KM2 ply is dependent on the way the change from the actual weave pattern to a solid element description is interpreted. The areal density of the experimental layup was quoted as  $5.22 \text{ kg/m}^2$  with a modeled effective thickness (not the true experimental thickness) of 3.63 mm given by Johnson et al. (1999) for the 23 plies. These constants force each ply thickness to be 0.1578 mm and the volumetric density for this thickness to be  $1.438 \text{ g/cm}^3$ . Since each actual ply was a plain weave of 850 denier yarn, this fact fixes the maximum total target thickness allowed. With 23 plies and 22 gaps between plies built in, this makes each gap 0.1391 mm wide to give a reasonable approximation of the total target thickness as 6.6896 mm, which was equal to the measured thickness of a 23-ply layup measured in the laboratory, within a small error band. It was thought that the solid elements with gaps between plies were required to minimize the effect of geometric nonproportionality on the simulated penetration process. One would encounter this effect by equating the 23 plies to some type of single-layer shell element description, for example.

Two quantities in Table 2 that definitely require an explanation for their origins are the Young's modulus and failure strain values. Shim et al. (2001) found, while conducting high strain-rate testing with the Split-Hopkinson Pressure Bar (SHPB), that the failure of Twaron fabric (similar to KM2 fabric) is highly strain-rate dependent with the tensile strength and modulus increasing with increasing strain rate, while the failure strain decreases with increasing strain rate. They also found that Twaron fabric failed in a more brittle manner as a function of increasing strain rate, which significantly reduced the amount of energy that could be absorbed by a particular yarn prior to its failure. This is consistent with the observed behavior described in the previous sentence. These experimental observations can be used to help describe the failure behavior of fabrics during ballistic penetration as follows. In a set of ballistic experiments, the strain rate experienced by the target material increases in some proportion to increasing projectile impact velocity, holding all other initial conditions constant. Thus, at higher impact velocities, the KM2 fabric should exhibit a higher Young's modulus and a lower strain to failure (see Table 2). Now, the Young's modulus and failure strains in Table 2 do not exactly fit the values given by Shim et al. (2001), but are extrapolated from their data. It was assumed, given the high strain rates achieved in the ballistic testing modeled in this report, that the yarns in the fabric weave could be thought to have elastic material properties to the point of failure with virtually no onset of plastic deformation. This assumption can be thought of as an elastic-perfectly brittle model. The highest modulus found for the Twaron fabric (more similar to Kevlar 29 fabric than to KM2 fabric) by Shim et al. (2001) was close to 0.74 Mbar at the highest testing strain-rate they used ( $495 \text{ s}^{-1}$ ). This was assumed to be a fair estimate corresponding to the strain-rate encountered on the high end of the striking velocity range of the

simulated ballistic tests with the KM2 fabric. However, KM2 fibers are somewhat tougher than Twaron or Kevlar 29 fibers, so the Shim et al. (2001) strain to failure of about 0.016 was increased to match the toughness-related increase in the ductile-to-brittle strain-to-failure criterion for the KM2 (failure strain = 0.025). Shim et al. (2001) found very low Young's moduli at the lowest end (quasi-static) of their strain-rate range (see their Figure 4). To reflect the strain-rate condition of a lower Young's modulus for a lower strain rate, a midrange-value Young's modulus was picked for the 200 and 400 m/s striking velocities as shown in Table 2. Based on the Shim et al. (2001) data values for strain-rate conditions approaching and equal to the quasi-static values for Twaron, a KM2 failure strain of 0.2 appeared to be reasonable. However, if actual SHPB data were ever obtained for KM2 fabric, the method for determining the Young's modulus and failure strain values in Table 2 would have to be readdressed.

The LS-DYNA-programmed  $V_s$  values were 200, 400, 600, 800, 1000, 1200, and 1400 m/s. The simulated penetration behavior for each  $V_s$  is visually summarized in Figures 2-9 as a product of the LS-POST software package.\* For scaling purposes in these figures, it must be remembered that the projectile diameter was 5.45 mm, but this value is directly scalable only in the y-direction, as the simulations have been rotated about the y-axis to enhance the view of the deformation of the projectile and the failure of the target material. With the 200 m/s  $V_s$ , five simulated plies were penetrated and only severe deformation without failure occurred in all remaining plies. Obviously, the condition that no part of the projectile exits the last ply was met exactly for a "no perforation" condition. For the 400 m/s  $V_s$ , significantly more simulated plies (16) were penetrated than at the 200 m/s  $V_s$ , which is consistent with the fact that deeper penetration occurs experimentally as the striking velocity increases; the "no perforation" condition was still met. For  $V_s$  of 600 m/s and above, the  $V_r$  was determined by tracking, in time, the velocity of the center rear node on the back of the RCC. When the projectile's rear surface velocity converged sufficiently to a constant velocity after penetration, that velocity was picked for the  $V_r$ .

### 2.3 EPIC Simulations

The EPIC-simulated  $V_s$  versus  $V_r$  points from Johnson et al. (1999) are shown in Figure 1 and Table 1. Comparisons to the LS-DYNA results can be made. For example, the difference between the  $V_r$  values for the 600 m/s  $V_s$  runs is not a major disparity, since any  $V_r$  in that vicinity has been shown experimentally to be a difficult number to interpret also. Hydrocodes do not predict  $V_r$  values at or near the experimentally determined  $V_{50}$ , a meta-stable point in the true penetration process, with accuracy any better than that found experimentally. Experimental anomalies occur near the  $V_{50}$  because of subtle shot-to-shot

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\* LS-POST Version 1.0, Livermore, CA: Livermore Software Technology Corporation.

**RCC(1.04GM); 0.02 CM/MICROSEC;23PLY KM2**

Time = 0

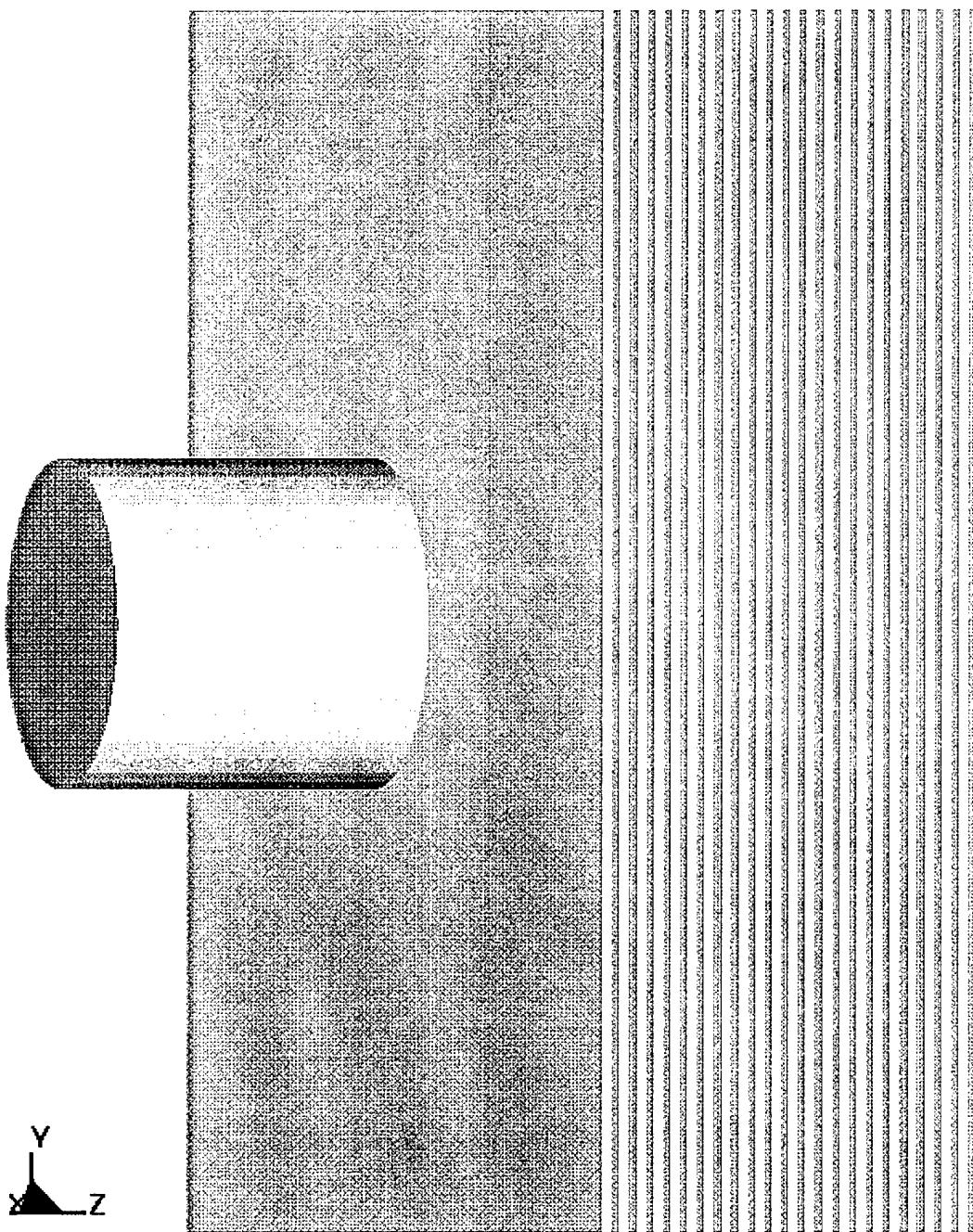


Figure 2. LS-DYNA RCC and target simulation grid prior to impact ( $V_s = 200$  m/s).

**RCC(1.04GM); 0.02 CM/MICROSEC;23PLY KM2**  
Time = 70



Figure 3. LS-DYNA simulation at 70  $\mu$ s into run showing damage up to the fifth ply ( $V_s = 200$  m/s).

**RCC(1.04GM); 0.04 CM/MICROSEC;23PLY KM2**

Time = 70

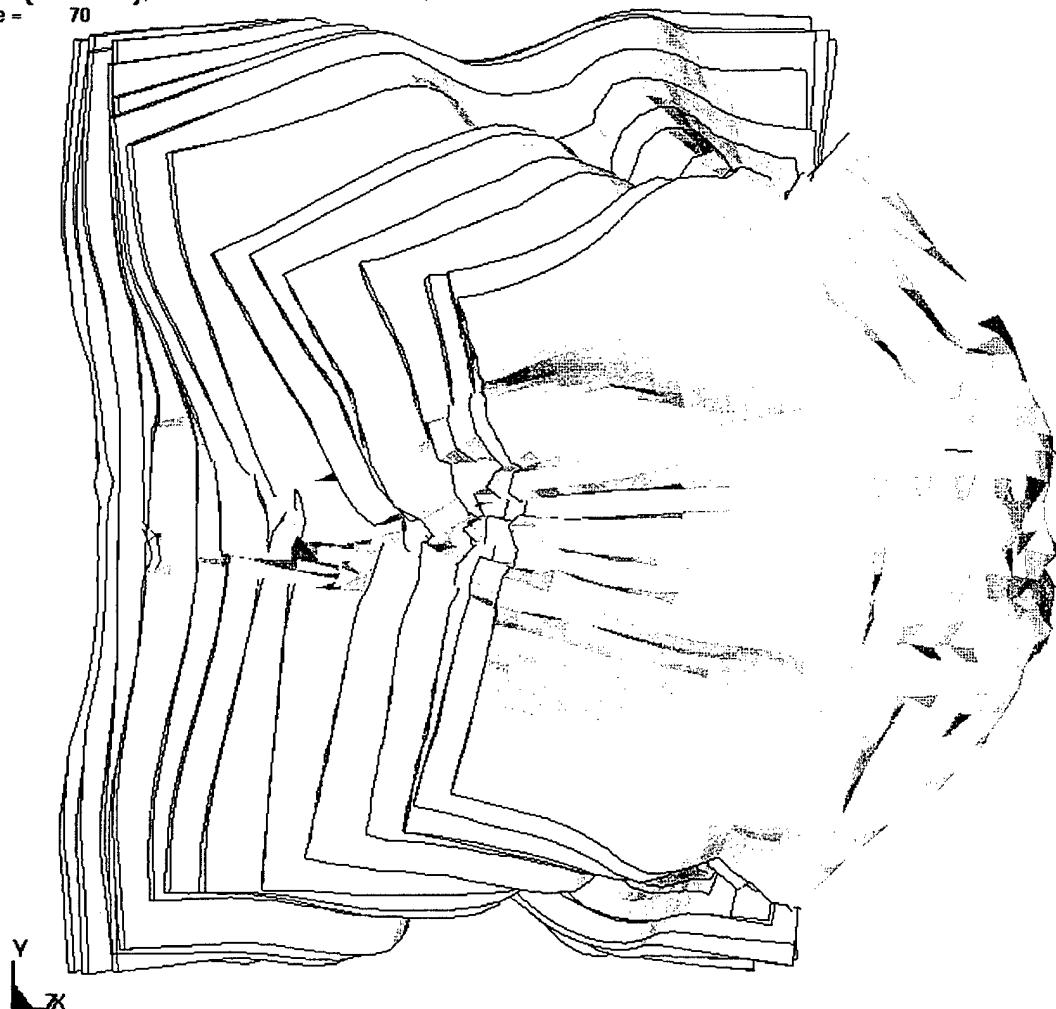


Figure 4. LS-DYNA simulation at 70  $\mu$ s into run showing damage up to the sixteenth ply ( $V_s = 400$  m/s).

RCC(1.04GM); 0.06 CM/MICROSEC; 23PLY KM2

Time = 30

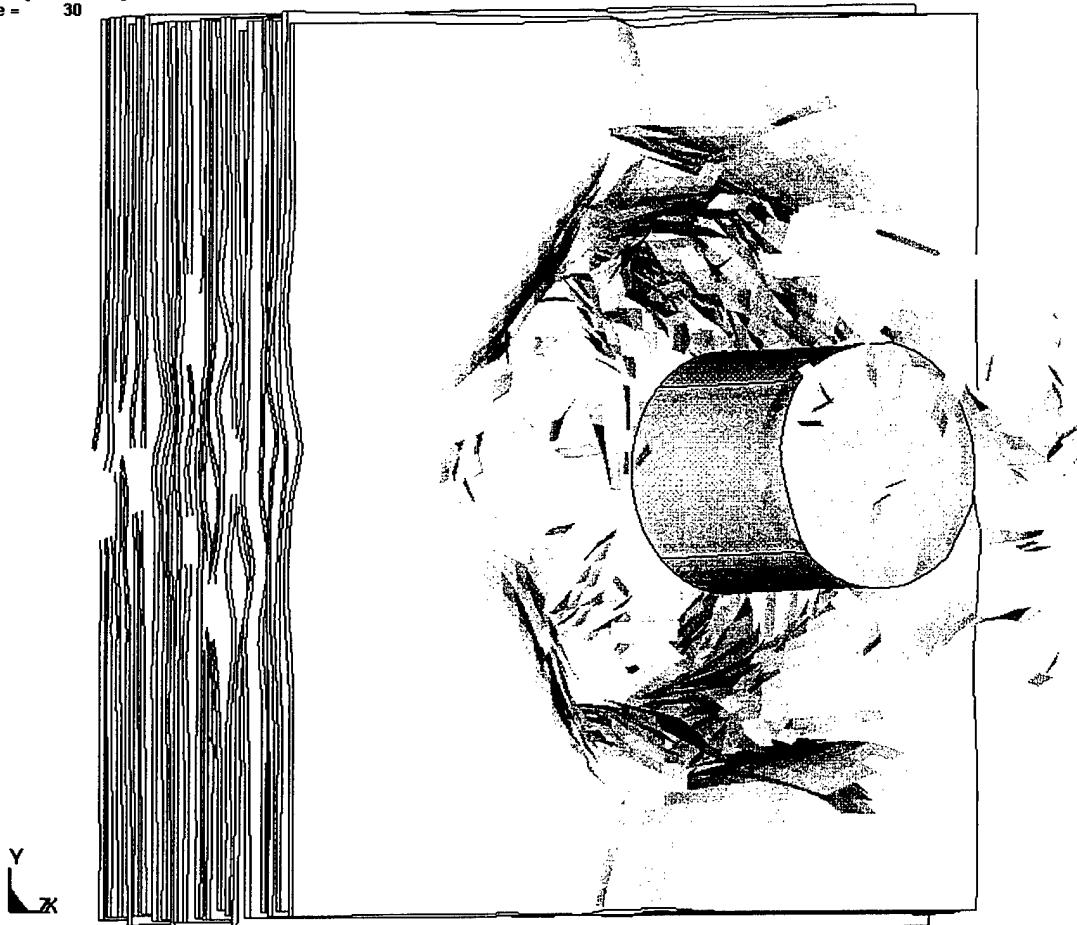


Figure 5. LS-DYNA simulation at 30  $\mu$ s into run ( $V_s = 600$  m/s).

RCC(1.04GM); 0.08 CM/MICROSEC; 23PLY KM2  
Time = 30

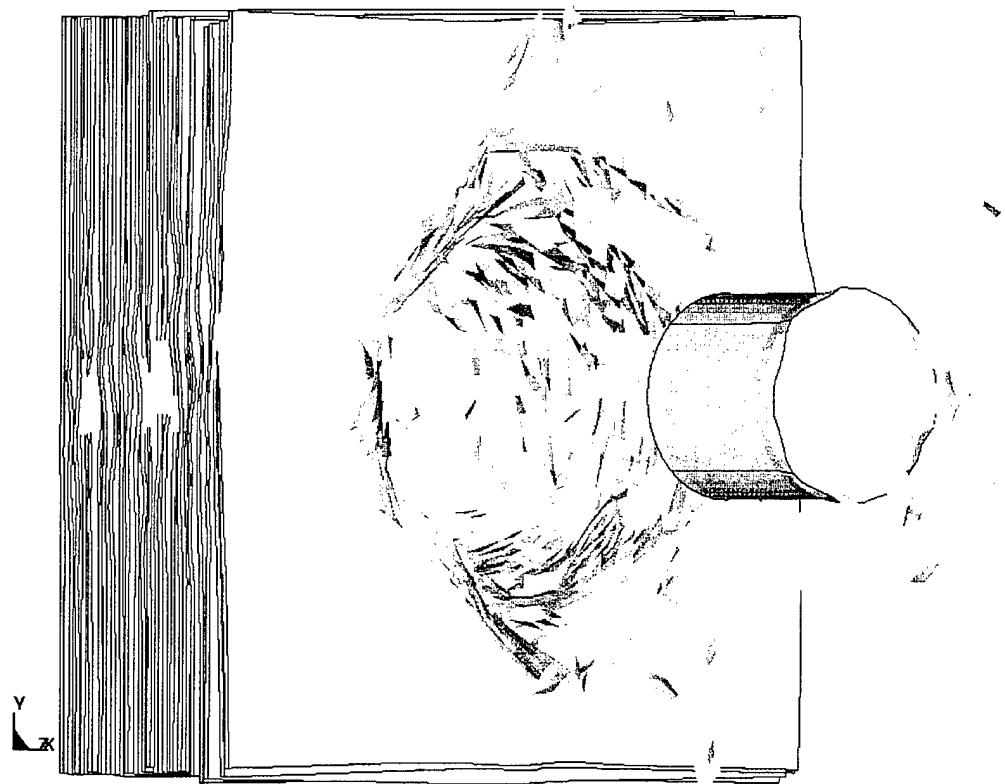


Figure 6. LS-DYNA simulation at 30  $\mu$ s into run ( $V_s = 800$  m/s).

RCC(1.04GM); 0.10 CM/MICROSEC; 23PLY KM2  
Time = 25

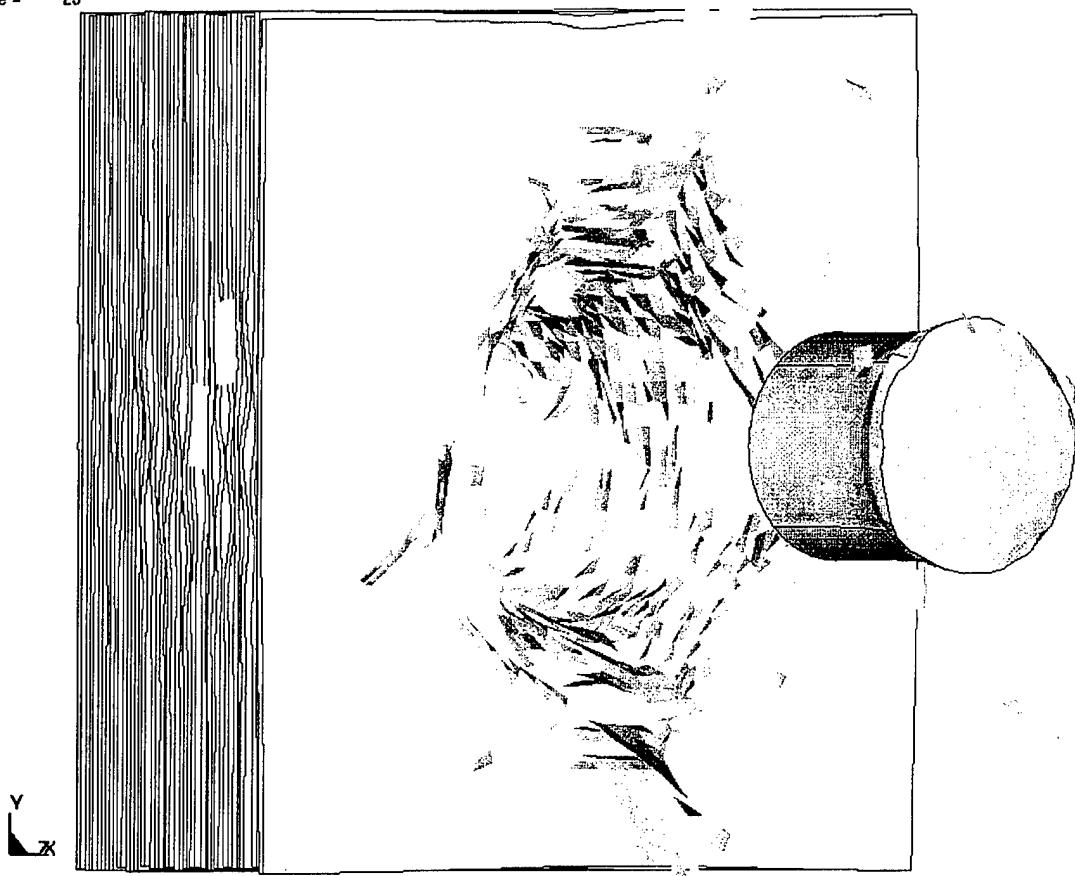


Figure 7. LS-DYNA simulation at 25  $\mu$ s into run ( $V_s = 1000$  m/s).

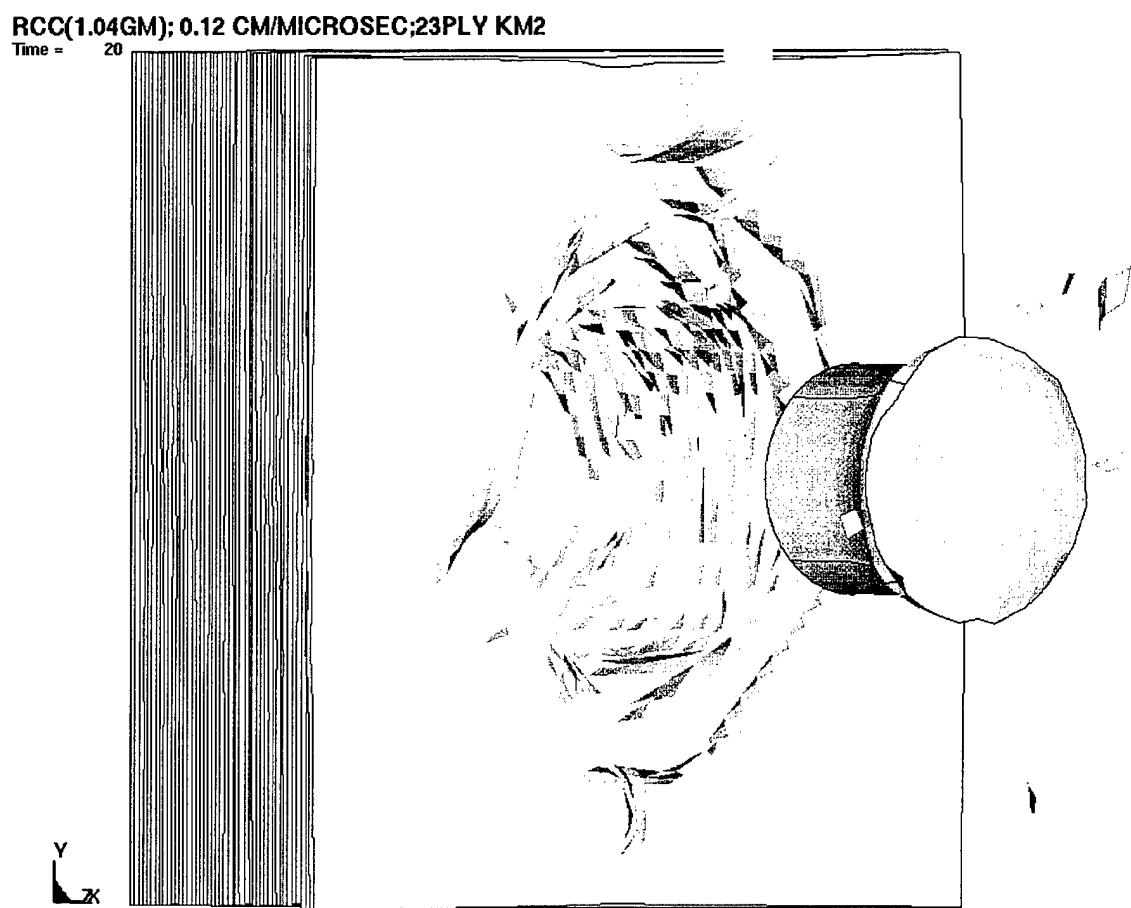


Figure 8. LS-DYNA simulation at 20  $\mu$ s into run ( $V_s = 1200$  m/s).

RCC(1.04GM); 0.14 CM/MICROSEC; 23PLY KM2

Time = 15

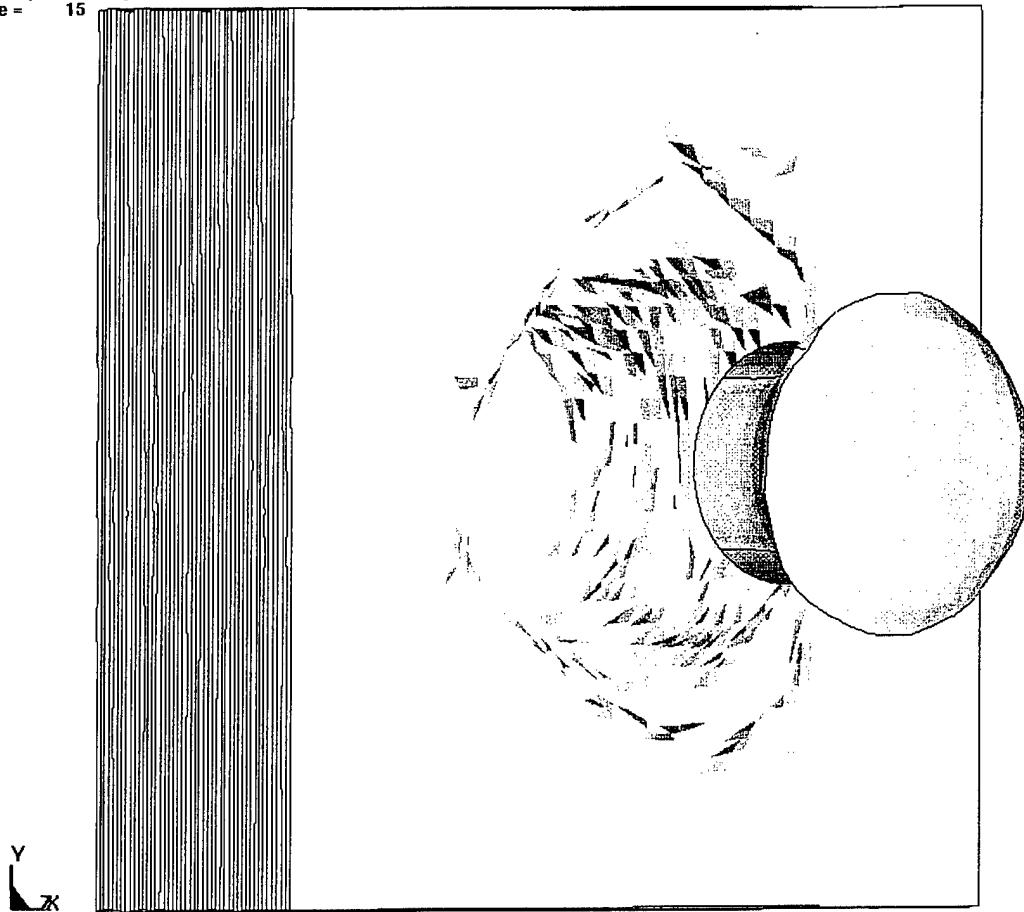


Figure 9. LS-DYNA simulation at 15  $\mu$ s into run ( $V_s = 1400$  m/s).

variations in the way real fabrics tear in the final penetration process. This effect leads to some penetrators being just caught by the last fabric ply or just making it through that ply with little velocity to spare, given the same  $V_s$ . The LS-DYNA computations are flexible, as they allow for the uncertainty of such behavior by letting key input material properties change as required, specifically the Young's modulus and failure strain in Table 2 in this case, accounting for this behavior. Actually, EPIC picked a  $V_r$  value that can be thought of as a  $V_0$  value.  $V_0$  is defined as the  $V_s$  at which no residual velocity can be obtained. Although EPIC predicted a  $V_0$  in this case,  $V_0$  is not usually obtained experimentally with exacting precision, so its determination to an overly precise number for comparison purposes should not be a computational goal.

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### 3. Summary

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The work here forms a baseline for the simulation of fabric penetration by fragment and bullet threats. Future plans include extending the LS-DYNA simulation techniques reported here to a study of 9-mm bullet impact on similar fabric layups. Also, more SHPB testing needs to be sponsored to assist in the process of defining increasingly accurate values for the Young's modulus and failure strain (as functions of strain rate) of KM2 and other ballistic fabrics of interest. This could lead to the development of analytical expressions describing Young's modulus and failure strain as functions of strain rate rather than the first-order discontinuous step model used in the present study. This report demonstrates a technique for reasonably describing the ballistic response of KM2 fabric using the LS-DYNA Lagrangian hydrocode. Using this technique, simulations can be performed to gain additional insight into understanding how the fabric components of armored vests resist ballistic penetration.

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#### 4. References

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- Department of the Army. *V<sub>50</sub> Ballistic Test for Armor.* MIL-STD-662E, Washington, DC, 27 May 1992.
- Flinn, R. A., and P. K. Trojan. *Engineering Materials and Their Applications.* Boston: Houghton Mifflin, pp. 61 and 72, 1975.
- Johnson, G. R., S. R. Beissel, and P. M. Cunniff. "A Computational Model for Fabrics Subjected to Ballistic Impact." *Proceedings of the 18th International Symposium on Ballistics,* pp. 962-969, San Antonio, TX, November 1999.
- Kolsky, H. *Stress Waves in Solids.* New York: Dover Publications, p. 201, 1963.
- Lyman, T. (editor). *Metals Handbook – 8th Edition, Volume 1: Properties and Selection of Materials.* Metals Park, OH: American Society for Metals, p. 798, 1961.
- Shim, V. P. W., C. T. Lim, and K. J. Foo. "Dynamic Mechanical Properties of Fabric Armour." *International Journal of Impact Engineering,* vol. 25, p. 1-15, 2001.

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**Appendix A. LS-Ingrid Input Deck for RCC and  
23-Ply Target**

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```

GRID 1.0 GM RCC AND 23 PLIES KM2
dn3d kw93
c Definition of Parts
start
c ijk notation (Part 1 - Impactor)
1 11;1 11;1 11;
c geometry
0.0545 -0.0545 0.0545 -0.0545 0.000 0.545
a 1 1 1 2 2 2 3 0.2725
C Assign a part number.
mate 1
end
start
c ijk notation (Part 2 - Ply 1)
1 41;1 41;1 2;
c geometry
1.0 -1.0 1.0 -1.0 0.58500 0.60078
c Assign a part number.
mate 2
end
start
c ijk notation (Part 3 - Ply 2)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 0.61469 0.63047
mate 3
end
start
c ijk notation (Part 4 - Ply 3)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 0.64438 0.66016
mate 4
end
start
c ijk notation (Part 5 - Ply 4)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 0.67407 0.68985
mate 5
end
start
c ijk notation (Part 6 - Ply 5)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 0.70376 0.71954
mate 6
end
start
c ijk notation (Part 7 - Ply 6)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 0.73345 0.74923
mate 7
end
start
c ijk notation (Part 8 - Ply 7)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 0.76314 0.77892

```

```

mate 8
end
start
c ijk notation (Part 9 - Ply 8)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 0.79283 0.80861
mate 9
end
start
c ijk notation (Part 10 - Ply 9)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 0.82252 0.83830
mate 10
end
start
c ijk notation (Part 11- Ply 10)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 0.85221 0.86799
mate 11
end
start
c ijk notation (Part 12 - Ply 11)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 0.88190 0.89768
mate 12
end
start
c ijk notation (Part 13 - Ply 12)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 0.91159 0.92737
mate 13
end
start
c ijk notation (Part 14 - Ply 13)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 0.94128 0.95706
mate 14
end
start
c ijk notation (Part 15 - Ply 14)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 0.97097 0.98675
mate 15
end
start
c ijk notation (Part 16 - Ply 15)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 1.00066 1.01644
mate 16
end
start
c ijk notation (Part 17 - Ply 16)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 1.03035 1.04613

```

```
mate 17
end
start
c ijk notation (Part 18 - Ply 17)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 1.06004 1.07582
mate 18
end
start
c ijk notation (Part 19 - Ply 18)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 1.08973 1.10551
mate 19
end
start
c ijk notation (Part 20 - Ply 19)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 1.11942 1.13520
mate 20
end
start
c ijk notation (Part 21 - Ply 20)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 1.14911 1.16489
mate 21
end
start
c ijk notation (Part 22 - Ply 21)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 1.17880 1.19458
mate 22
end
start
c ijk notation (Part 23 - Ply 22)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 1.20849 1.22427
mate 23
end
start
c ijk notation (Part 24 - Ply 23)
1 41;1 41;1 2;
1.0 -1.0 1.0 -1.0 1.23818 1.25396
mate 24
end
end
```

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**Appendix B. Abbreviated LS-DYNA Input Deck for RCC  
Impacting 23-Ply Target ( $V_s = 200$  m/s)**

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*KEYWORD
*TITLE
RCC(1.04gm); 0.02 cm/microsec;23ply KM2
$      mass, length,      time, force, pressure & modulus & stress,      energy
$ Unit=   gm,          cm, microsec, 1e+07 N,                               Mbar, 1e+07 N-cm
$
$-----1-----2-----3-----4-----5-----6-----7-----8
$-----+
*CONTROL_TIMESTEP
$ dtinit    tssfac
 0.0000    0.7000
*CONTROL_TERMINATION
$ endtime
 70.0
*CONTROL_CONTACT
$ slsfac
 1.0
$ usrstr
 0
*CONTROL_ENERGY
$ hgen      rwen
 2        2
*CONTROL_OUTPUT
$ npopt     neecho
 0        0
$
*DATABASE_EXTENT_BINARY
$ neiph     neips    maxint    strflg    sigflg    epsflg    rltflg    engflg
 0         0         0         1         0         0         0         0
$
$ cmpflg    ieverb    beamip    dcomp    shge    stsz    n3thdt
 0         0         0         0         0         0         0
$
*DATABASE_BINARY_D3PLOT
$ dt/cycl
 5.0
*DATABASE_BINARY_D3THDT
$ dt/cycl
 5.0
*DATABASE_MATSUM
$ dt/cycl
 1.0
*DATABASE_HISTORY_NODE
$ node id1      id2      id3      id4      id5      id6      id7      id8
 1         61
*DATABASE_NODOUT
$ dt/cycl
 1.0
*DATABASE_ELOUT
$ dt/cycl
 1.0
*DATABASE_NODFOR
$ dt/cycl
 1.0
*DATABASE_GLSTAT
$ dt/cycl
 1.0
*DATABASE_TRHIST
$ dt/cycl
 1.0
*DATABASE_TRACER
$ start dt L(0)/E(1)      x      y      z
 0.0       0       0.0      0.0      0.0
$
$slave impactor to all plies $$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$-----+
*CONTACT_ERODING_SURFACE_TO_SURFACE
$ ssid      msid      sstyp      mstyp

```

```

      1          2          3          3
$    fric
$    0.0
$    sfs
$    1.0
$    isym    erosop
$        1        1
$ 
*$CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
$        1        3        3        3
$    fric
$    0.0
$    sfs
$    1.0
$    isym    erosop
$        1        1
$ 
*$CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
$        1        4        3        3
$    fric
$    0.0
$    sfs
$    1.0
$    isym    erosop
$        1        1
$ 
*$CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
$        1        5        3        3
$    fric
$    0.0
$    sfs
$    1.0
$    isym    erosop
$        1        1
$ 
*$CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
$        1        6        3        3
$    fric
$    0.0
$    sfs
$    1.0
$    isym    erosop
$        1        1
$ 
*$CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
$        1        7        3        3
$    fric
$    0.0
$    sfs
$    1.0
$    isym    erosop
$        1        1
$ 
*$CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
$        1        8        3        3
$    fric
$    0.0
$    sfs
$    1.0
$    isym    erosop
$        1        1
$ 

```

```

*CONTACT_ERODING_SURFACE_TO_SURFACE
$ ssid      msid      sstyp      mstyp
    1          9          3          3
$ fric
  0.0
$ sfs
  1.0
$ isym    erosop
    1          1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$ ssid      msid      sstyp      mstyp
    1         10          3          3
$ fric
  0.0
$ sfs
  1.0
$ isym    erosop
    1          1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$ ssid      msid      sstyp      mstyp
    1         11          3          3
$ fric
  0.0
$ sfs
  1.0
$ isym    erosop
    1          1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$ ssid      msid      sstyp      mstyp
    1         12          3          3
$ fric
  0.0
$ sfs
  1.0
$ isym    erosop
    1          1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$ ssid      msid      sstyp      mstyp
    1         13          3          3
$ fric
  0.0
$ sfs
  1.0
$ isym    erosop
    1          1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$ ssid      msid      sstyp      mstyp
    1         14          3          3
$ fric
  0.0
$ sfs
  1.0
$ isym    erosop
    1          1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$ ssid      msid      sstyp      mstyp
    1         15          3          3
$ fric
  0.0
$ sfs
  1.0
$ isym    erosop

```

```

          1         1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      1        16        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      1        17        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      1        18        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      1        19        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      1        20        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      1        21        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      1        22        3        3
$    fric
      0.0
$    sfs

```

```

      1.0
$    isym    erosop
      1      1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      1        23        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1      1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      1        24        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1      1
$
$initiate master-slave routine for each ply $$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      2        3        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1      1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      2        4        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1      1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      3        4        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1      1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      3        5        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1      1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp

```

```

        4      5      3      3
$    fric
$    0.0
$    sfs
$    1.0
$    isym    erosop
$        1        1
$
*$CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
$        4        6        3        3
$    fric
$    0.0
$    sfs
$    1.0
$    isym    erosop
$        1        1
$
*$CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
$        5        6        3        3
$    fric
$    0.0
$    sfs
$    1.0
$    isym    erosop
$        1        1
$
*$CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
$        5        7        3        3
$    fric
$    0.0
$    sfs
$    1.0
$    isym    erosop
$        1        1
$
*$CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
$        6        7        3        3
$    fric
$    0.0
$    sfs
$    1.0
$    isym    erosop
$        1        1
$
*$CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
$        6        8        3        3
$    fric
$    0.0
$    sfs
$    1.0
$    isym    erosop
$        1        1
$
*$CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
$        7        8        3        3
$    fric
$    0.0
$    sfs
$    1.0
$    isym    erosop
$        1        1
$
```

```

*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      7          9          3          3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1          1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      8          9          3          3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1          1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      8          10         3          3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1          1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      9          10         3          3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1          1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      9          11         3          3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1          1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      10         11         3          3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1          1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      10         12         3          3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop

```

```

          1          1
$ *CONTACT_ERODING_SURFACE_TO_SURFACE
$   ssid      msid      sstyp      mstyp
$     11        12        3        3
$   fric
$     0.0
$   sfs
$     1.0
$   isym      erosop
$     1        1
$ *CONTACT_ERODING_SURFACE_TO_SURFACE
$   ssid      msid      sstyp      mstyp
$     11        13        3        3
$   fric
$     0.0
$   sfs
$     1.0
$   isym      erosop
$     1        1
$ *CONTACT_ERODING_SURFACE_TO_SURFACE
$   ssid      msid      sstyp      mstyp
$     12        13        3        3
$   fric
$     0.0
$   sfs
$     1.0
$   isym      erosop
$     1        1
$ *CONTACT_ERODING_SURFACE_TO_SURFACE
$   ssid      msid      sstyp      mstyp
$     12        14        3        3
$   fric
$     0.0
$   sfs
$     1.0
$   isym      erosop
$     1        1
$ *CONTACT_ERODING_SURFACE_TO_SURFACE
$   ssid      msid      sstyp      mstyp
$     13        14        3        3
$   fric
$     0.0
$   sfs
$     1.0
$   isym      erosop
$     1        1
$ *CONTACT_ERODING_SURFACE_TO_SURFACE
$   ssid      msid      sstyp      mstyp
$     13        15        3        3
$   fric
$     0.0
$   sfs
$     1.0
$   isym      erosop
$     1        1
$ *CONTACT_ERODING_SURFACE_TO_SURFACE
$   ssid      msid      sstyp      mstyp
$     14        15        3        3
$   fric
$     0.0
$   sfs
$     1.0

```

```

$      isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$      ssid     msid     sstyp     mstyp
      14        16        3        3
$      fric
      0.0
$      sfs
      1.0
$      isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$      ssid     msid     sstyp     mstyp
      15        16        3        3
$      fric
      0.0
$      sfs
      1.0
$      isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$      ssid     msid     sstyp     mstyp
      15        17        3        3
$      fric
      0.0
$      sfs
      1.0
$      isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$      ssid     msid     sstyp     mstyp
      16        17        3        3
$      fric
      0.0
$      sfs
      1.0
$      isym    erosop
      1        1
*
*CONTACT_ERODING_SURFACE_TO_SURFACE
$      ssid     msid     sstyp     mstyp
      16        18        3        3
$      fric
      0.0
$      sfs
      1.0
$      isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$      ssid     msid     sstyp     mstyp
      17        18        3        3
$      fric
      0.0
$      sfs
      1.0
$      isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$      ssid     msid     sstyp     mstyp
      17        19        3        3
$      fric
      0.0
$      sfs

```

```

      1.0
$    isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      18        19        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      18        20        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      19        20        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      19        21        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      20        21        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      20        22        3        3
$    fric
      0.0
$    sfs
      1.0
$    isym    erosop
      1        1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$    ssid      msid      sstyp      mstyp
      21        22        3        3
$    fric

```

```

          0.0
$      sfs
1.0
$      isym    erosop
     1       1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$      ssid      msid      sstyp      mstyp
     21       23       3         3
$      fric
0.0
$      sfs
1.0
$      isym    erosop
     1       1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$      ssid      msid      sstyp      mstyp
     22       23       3         3
$      fric
0.0
$      sfs
1.0
$      isym    erosop
     1       1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$      ssid      msid      sstyp      mstyp
     22       24       3         3
$      fric
0.0
$      sfs
1.0
$      isym    erosop
     1       1
$
*CONTACT_ERODING_SURFACE_TO_SURFACE
$      ssid      msid      sstyp      mstyp
     23       24       3         3
$      fric
0.0
$      sfs
1.0
$      isym    erosop
     1       1
$
*INITIAL_VELOCITY_GENERATION
$      sid      styp      omega      vx        vy        vz
     1           1
$      xc       yc       zc
0.02
$
*SET_PART
$      setid
     1
$      pid1
     1
$
*PART
$      pid      sid      mid
16 gr RCC
     1       1       1
1st ply of KM2
     2       1       2
2nd ply of KM2
     3       1       2
3rd ply of KM2
     4       1       2

```

```

4th ply of KM2
      5       1       2
5th ply of KM2
      6       1       2
6th ply of KM2
      7       1       2
7th ply of KM2
      8       1       2
8th ply of KM2
      9       1       2
9th ply of KM2
     10      1       2
10th ply of KM2
     11      1       2
11th ply of KM2
     12      1       2
12th ply of KM2
     13      1       2
13th ply of KM2
     14      1       2
14th ply of KM2
     15      1       2
15th ply of KM2
     16      1       2
16th ply of KM2
     17      1       2
17th ply of KM2
     18      1       2
18th ply of KM2
     19      1       2
19th ply of KM2
     20      1       2
20th ply of KM2
     21      1       2
21st ply of KM2
     22      1       2
22nd ply of KM2
     23      1       2
23rd ply of KM2
     24      1       2
$
$Type 3 - Steel Impactor$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
*MAT_PLASTIC_KINEMATIC
$    mid      rho      e      pr      sigy      etan      beta
$      1      7.87   2.068395     0.29   0.010342      0.0      0.0
$    src      srp      fs
         9999.0
$Type 1 - Fabric$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
*MAT_ELASTIC
$    mid      rho      e      pr      da      db      k
$      2      1.438   0.08325     0.2
$
$EROSION FOR FABRIC - TYPE1$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
*MAT_ADD_EROSION
$    mid      excl
$      2      9999.0
$    pfail    sigp1      sigvm      epsp1      epssh      sigth      impulse
$    99.0     99.0      99.0      0.200     99.0      99.0      99.0
$
*$SECTION_SOLID
$    sid      elform
$      1          1
$
$-----1-----2-----3-----4-----5-----6-----7-----8
$
*NODE
$node id      x          y          z          tc          rc
$      1 1.926866323E-01 1.926866323E-01 0.000000000E+00      0          0

```

2	1.601715088E-01	2.204571813E-01	0.000000000E+00	0	0
3	1.237124354E-01	2.427993417E-01	0.000000000E+00	0	0
4	8.420714736E-02	2.591629624E-01	0.000000000E+00	0	0
5	4.262839630E-02	2.691451609E-01	0.000000000E+00	0	0
6-1	0.056444709E-08	2.725000679E-01	0.000000000E+00	0	0
7-4	2.62841865E-02	2.691451609E-01	0.000000000E+00	0	0
8-8	420717716E-02	2.591629922E-01	0.000000000E+00	0	0
9-1	2.37124726E-01	2.427993566E-01	0.000000000E+00	0	0
10-1	6.01715535E-01	2.204572111E-01	0.000000000E+00	0	0
11-1	9.26866323E-01	1.926866323E-01	0.000000000E+00	0	0
12	2.204571813E-01	1.601715088E-01	0.000000000E+00	0	0

NOTE: THE MISSING NODES IN THIS ABBREVIATED DECK ARE HERE IN THE ACTUAL RUN

78646-4.499999881E-01-1.000000000E+00	1.253960252E+00	0	0
78647-5.000000000E-01-1.000000000E+00	1.253960252E+00	0	0
78648-5.500000119E-01-1.000000000E+00	1.253960252E+00	0	0
78649-6.000000238E-01-1.000000000E+00	1.253960252E+00	0	0
78650-6.499999762E-01-1.000000000E+00	1.253960252E+00	0	0
78651-6.999999881E-01-1.000000000E+00	1.253960252E+00	0	0
78652-7.500000000E-01-1.000000000E+00	1.253960252E+00	0	0
78653-8.000000119E-01-1.000000000E+00	1.253960252E+00	0	0
78654-8.500000238E-01-1.000000000E+00	1.253960252E+00	0	0
78655-8.999999762E-01-1.000000000E+00	1.253960252E+00	0	0
78656-9.499999881E-01-1.000000000E+00	1.253960252E+00	0	0
78657-1.000000000E+00-1.000000000E+00	1.253960252E+00	0	0

\*ELEMENT\_SOLID

1	1	1	2	13	12	122	123	134	133
2	1	2	3	14	13	123	124	135	134
3	1	3	4	15	14	124	125	136	135
4	1	4	5	16	15	125	126	137	136
5	1	5	6	17	16	126	127	138	137
6	1	6	7	18	17	127	128	139	138
7	1	7	8	19	18	128	129	140	139
8	1	8	9	20	19	129	130	141	140
9	1	9	10	21	20	130	131	142	141
10	1	10	11	22	21	131	132	143	142
11	1	12	13	24	23	133	134	145	144
12	1	13	14	25	24	134	135	146	145

NOTE: THE MISSING SOLID ELEMENTS IN THIS ABBREVIATED DECK ARE HERE IN THE ACTUAL RUN

37789	24	76923	76924	76965	76964	78604	78605	78646	78645
37790	24	76924	76925	76965	76965	78605	78606	78647	78646
37791	24	76925	76926	76967	76966	78606	78607	78648	78647
37792	24	76926	76927	76968	76967	78607	78608	78649	78648
37793	24	76927	76928	76969	76968	78608	78609	78650	78649
37794	24	76928	76929	76970	76969	78609	78610	78651	78650
37795	24	76929	76930	76971	76970	78610	78611	78652	78651
37796	24	76930	76931	76972	76971	78611	78612	78653	78652
37797	24	76931	76932	76973	76972	78612	78613	78654	78653
37798	24	76932	76933	76974	76973	78613	78614	78655	78654
37799	24	76933	76934	76975	76974	78614	78615	78656	78655
37800	24	76934	76935	76976	76975	78615	78616	78657	78656

\*END

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<b>13. ABSTRACT</b> (Maximum 200 words)  A study was conducted to examine the terminal effects of a 1.0-g steel RCC impacting 23 plies of KM2 fabric using the LS-DYNA Lagrangian hydrocode. The simulated impact velocities were 200, 400, 600, 800, 1000, 1200, and 1400 m/s. The fabric was a plain weave of 850 denier yarn. The LS-DYNA-simulated $V_s$ versus $V_r$ data points generated at the U.S. Army Research Laboratory (ARL) were compared to both experimental data and EPIC-generated data. Also, the LS-POST software package was used to view the simulated physical descriptions of the penetrator and target at various stages of the penetration process.			<b>12b. DISTRIBUTION CODE</b>			
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